

1 **TITLE:** INFLUENCE OF MUSCLE ARCHITECTURE ON MAXIMAL REBOUNDING IN  
2 YOUNG BOYS

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4 **BRIEF RUNNING HEAD:** MUSCLE ARCHITECTURE AND REBOUNDING IN BOYS

5

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35 ABSTRACT

36 The aims of the current study were to i) investigate differences in maximal rebound jump  
37 kinetics in boys at different stages of maturity, and ii) determine the relationship of muscle  
38 architecture characteristics to maximal rebound jump kinetics. One hundred twenty-seven  
39 male, secondary school children were categorised into maturity groups (pre-, circa- and post-  
40 PHV) based on their maturity offset value. Muscle architecture of the gastrocnemius medialis  
41 (GM) and vastus lateralis (VL) was evaluated at rest using B-Mode ultrasonography.  
42 Participants then performed maximal rebound jumps quantified on a force platform. There  
43 were moderate to large, differences across all maturity groups for peak ground reaction force  
44 (GRF), impulse measures and average power variables ( $d = 0.73 - 2.67; p < 0.05$ ). GM and VL  
45 muscle thickness explained between 38.5-55.8% of the variance in peak force, impulse and  
46 power variables, however muscle architecture was less important determinant of contact time,  
47 jump height, reactive strength index (RSI), rate of force development (RFD), eccentric  
48 velocity, concentric velocity, and allometrically scaled measures (3.3 – 17.2%). The current  
49 results indicate that the majority of kinetics employed during maximal vertical rebounding are  
50 greater in more mature boys. Furthermore, maturational increases in GM muscle architecture  
51 appears important for maximal vertical jumping, and are specifically associated with increased  
52 force, power and impulse measures. Practically, these findings may underline benefits in  
53 targeting resistance training activities that are focused to increase lower limb muscle mass to  
54 positively influence maximal rebounding kinetics in young boys.

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59 KEY WORDS: Fascicle Length, Muscle Thickness, Hopping, Jumping, Youth, Maturation

## 60 INTRODUCTION

61 The stretch-shortening cycle (SSC) is a naturally occurring muscle action that involves an  
62 initial lengthening (eccentric action) prior to a subsequent shortening (concentric action) of the  
63 same muscle (29). The SSC action is fundamental to most tasks, including jumping and  
64 sprinting, which are common in both active play and competitive sports (31). However, SSC  
65 function in youth has often been assessed using basic countermovement vertical jump tests  
66 which, due to extended ground contact times and lack of pre-activation and rapid transition  
67 from stretch to shortening, reflect slow-SSC function (21). The maximal vertical rebound test  
68 may provide a more useful model of functional-SSC behaviour, due to the rapid and brief  
69 eccentric actions and shorter ground contact times (21). The maximal rebound test consists of  
70 self-regulated repeated jumps in place, and is cued to ensure athletes jump for maximal height  
71 with minimal ground contact time. Compared to sub-maximal hopping, where subjects rebound  
72 in time to a metronome, maximal hopping results in a lower rebounding frequency, increased  
73 jump heights and ground contact times (due to greater angular displacements at the hips, knees  
74 and ankles), and reduced stiffness (22).

75

76 Innate SSC development throughout childhood and adolescence enables children to jump  
77 higher (33) and sprint faster (24) as they mature. Research examining the effects of maturation  
78 on maximal vertical rebounding is sparse; although recent research has suggested that reactive  
79 strength index (RSI; calculated as jump height divided by ground contact time) in both a 20  
80 cm and 40 cm drop jump is better in more mature boys (6). However, using standardised drop  
81 jump heights fails to account for individual differences in reactive strength capabilities and any  
82 ‘optimal’ stimulus is likely to be transient in nature (1). Therefore, the use of maximal  
83 rebounding has become more popular (18). For example, through the use of the maximal 5-  
84 rebound vertical jump test, there is an increase in reactive strength index (RSI) performance in

85 boys between the ages of 10 and 16 years (20), with the largest increase in performance  
86 occurring between the ages of 10 and 11 years (20). However, the use of contact mats for the  
87 analysis of SSC function limited this study to only reporting performance-oriented variables  
88 (i.e. jump height, contact time, and RSI); therefore, the influence of underlying kinetics on SSC  
89 function during maximal rebounding in youth remains is not fully delineated (20).

90

91 Improvements in maximal rebound jump performance with maturation may be due to increases  
92 in neural factors, demonstrated by evidence that 15-year-old boys produce significantly greater  
93 levels of pre load muscle activation compared to 9- and 12-year olds during maximal rebound  
94 jumping (22). Increased preactivation increases joint stiffness, and reduces ground contact  
95 times, resulting in a more efficient SSC action during a rebound jump (34). Beyond neural  
96 influences, structural factors may also underlie improvements in maximal vertical rebounding  
97 performance throughout maturation, as, children have shown a smaller tendon excursion, and  
98 greater muscle length changes compared to adults during rebound tasks at different frequencies  
99 (39). The inability to create the required muscle stiffness to resist deformation reduces tendon  
100 excursion, resulting in less storage and return of elastic energy and therefore less efficient force  
101 generation during sport movements (39). Children may have less efficient muscle activation  
102 strategies and a reduced ability to create muscle stiffness during rebound tasks, resulting in  
103 inferior performance (39). Considering the arrangement of the fascicle within a muscle fibre  
104 and its influence on a global muscle's function (5), the specific muscular architecture control  
105 the ability to perform maximal vertical rebounding in youth, but to date this notion remains  
106 unsubstantiated.

107

108 Muscle architecture is typically characterised by parameters such as fascicle length, pennation  
109 angle and cross-sectional area (2, 19), and these muscle architecture characteristics develop

110 naturally throughout childhood and adolescence (17, 32). Muscle architecture has direct  
111 association with countermovement jump (CMJ) performance in youth (35, 37) and thickness  
112 of the gastrocnemius medialis and vastus lateralis muscles are associated with a greater  
113 performance in the eccentric phase of the CMJ in all stages of maturation in young boys (33).  
114 Specifically, VL muscle thickness and fascicle length are associated with greater jump height  
115 and relative peak power output in post-PHV boys (33) and increases in VL muscle thickness  
116 during natural growth and maturation is postulated as a key driver for increases in jump  
117 performance in male youth (33). While muscle thickness of the ankle and knee extensors are  
118 clearly important determinants for CMJ performance in young boys, it is yet to be determined  
119 how muscle architecture influences the kinetics of maximal jump rebounding.

120

121 Therefore, the aims of this study were to i) investigate differences in maximal rebounding  
122 kinetics in boys at different stages of maturity, and ii) determine the strength of relationships  
123 between maximal rebounding kinetics and muscle architecture characteristics. In light of  
124 previous studies, the hypotheses for the study were: i) post-PHV subjects would have greater  
125 force, impulse and power values across all kinetic variables during maximal rebound jumping,  
126 compared with their less mature counterparts and ii) muscle thickness will be the specific  
127 muscle architecture characteristic that determines maximal rebounding kinetic performance.

128

## 129 METHOD

### 130 **Experimental Approach to the Problem**

131 This study used a cross-sectional design to assess the differences in maximal rebounding  
132 performance between pre-, circa-, and post-PHV boys. Additionally, muscle architecture  
133 characteristics (muscle thickness, pennation angle and fascicle length) of both the GM and VL  
134 were derived using ultrasonography. A one-way ANOVA was used to identify differences in

135 force-time characteristics between pre-, circa-, and post-PHV cohorts during maximal  
136 rebounding, while Pearson correlation coefficients and multiple stepwise regression analyses  
137 were used to examine the relationships between muscle architecture characteristics and force-  
138 time characteristics of maximal rebounding.

139

## 140 **Subjects**

141 One hundred and twenty-seven male secondary school children in the United Kingdom  
142 volunteered to participate in the study. A priori power analysis was conducted (GPower,  
143 v3.1.9.4) using previously published means and standard deviations of RSI across pre-, circa,  
144 and post-PHV (23) indicating the required sample size for the current study would need to be  
145 90 subjects (30 per maturation group) to achieve a statistical power of 0.8 for detecting a  
146 moderate effect size (0.6\* standard deviation). All participants were free from injury for the 6  
147 months prior to the study and were involved in regular sport and physical education-based  
148 activity programmes, but were not receiving formal strength and conditioning support. Written  
149 parental consent and participant assent were obtained from all participants prior to the study  
150 commencing. Ethical approval for the study was granted by the Universities Research Ethics  
151 Committee (15/4/01R) in accordance with the declaration of Helsinki.

152

## 153 **Procedures**

154 All participants attended their usual physical education lessons as part of their school  
155 curriculum, where all testing took place. Participants were asked to refrain from strenuous  
156 exercise at least 48 hours prior to testing.

157

158 *Maturity status:* Biological maturity was assessed non-invasively by incorporating measures  
159 of body mass (kg), standing height (cm) and seated height (cm), measured using electronic

160 scales (SECA 770, Vogel and Halke, Germany) and a stadiometer (SECA 321, Vogel and  
161 Halke, Germany) respectively, into a sex-specific regression equation to predict age from peak  
162 height velocity (PHV) (26). For the between-maturity group analysis, due to the error in the  
163 maturity offset prediction equation, participants with a maturity offset between -1.0 to -0.5  
164 years, or +0.5 to +1.0 years were eliminated from the study (n = 28) to ensure three distinct  
165 maturity groups (pre-, circa- and post-PHV). The pre-PHV group included all participants with  
166 a maturity offset of <-1.0, -0.5 – 0.5 were classified as circa-PHV, and >+1.0 classified as post-  
167 PHV (see *table 1*). For the regression analyses all 127 subjects were included (mean  $\pm$  SD -  
168 age:  $13.73 \pm 1.42$  years; height:  $163.61 \pm 11.13$  cm; body mass:  $55.28 \pm 15.05$  kg; maturity  
169 offset:  $-0.22 \pm 1.50$  years).

170

171 **\*\*\* Table 1 inserted near here \*\*\***

172

173 *Muscle Architecture:* Muscle structure of the GM and VL were measured with B-Mode  
174 ultrasonography (Vivid E9, GE Healthcare, Chalfont St Giles, UK) with a 45-mm linear array  
175 probe. To measure the GM, participants laid prone on a massage couch with legs fully  
176 extended, and ankle positioned at approximately 90° relative to the shank, unsupported and  
177 unloaded (32). For the imaging of the VL, participants lay supine with the knee fully extended  
178 (anatomical zero) (12, 32). For the VL muscle, the ultrasound derived image was taken at 50%  
179 of the distance between the greater trochanter and the lateral epicondyle of the femur (35) and  
180 the GM image was taken at 30% of the distance from the popliteal crease to the centre of the  
181 lateral malleolus (16). The ultrasound scanning protocol provides moderate to excellent intra-  
182 rater reliability in young boys (32). Subsequent analysis of images was carried out using open-  
183 source image analysis software (Image J, National Institute of Health, Bethesda, MD, USA) to

184 identify muscle thickness, pennation angle, and fascicle length (32). Each ultrasound image  
185 was measured three times, with the average value for each variable used for analysis.

186

187 *Maximal vertical rebound test:* Participants completed a standardized 10-minute dynamic  
188 warm-up inclusive of three minutes of submaximal multidirectional running and seven minutes  
189 of light dynamic mobilization and activation exercises targeting the main muscle groups of the  
190 lower extremities. Following the warm-up, participants performed practice attempts of the  
191 maximal rebound jump protocol as the principal researcher qualitatively evaluated the task  
192 performance competency. Once technical competence was achieved, participants performed  
193 the maximal 5-rebound jump test (21) on a force platform (AMTI, Boston, MA) sampling at  
194 1000 Hz. Participants were instructed to stand still for the initial 1 second of the data-collection  
195 period (28) to allow for the determination of body weight. Subjects were instructed to keep  
196 their hands on their hips whilst aiming to maximise jump height and minimise ground contact  
197 time. The first jump in each trial was a countermovement jump, and consequently was excluded  
198 for analyses, with the remaining four jumps aggregated and averaged each trial. Within-session  
199 reliability was determined using measures quantified from the three rebound jump trials on the  
200 same day. For the between-maturity group and correlation analyses, the three trials were  
201 averaged and used for further analysis. The raw vertical force–time data for each trial were  
202 exported as a text file and analysed using a customised Microsoft Excel spreadsheet via  
203 Microsoft Excel for Mac (v.16). Ground reaction force data was smoothed using a fourth order  
204 recursive low-pass Butterworth filter with a cut off of 30 Hz and relevant outcomes variables  
205 calculated are detailed in *table 2*. Peak force, eccentric and concentric impulse, and eccentric  
206 and concentric average power were allometrically scaled to bodyweight to account for the non-  
207 linear relationship between muscular strength and body size. Kinetic data and bodyweight were  
208 log transformed and then entered into the linear regression models. The beta component of the



209 regression equation was subsequently used as the allometric scaling exponent. A Pearson  
210 product moment correlation coefficient was computed to confirm that the scaling exponent  
211 sufficiently controlled for bodyweight (7).

212

213 **\*\*\* Table 2 inserted near here \*\*\***

214

## 215 **Statistical Analyses**

216 Descriptive statistics (means  $\pm$  standard deviations) were calculated for all maximal rebound  
217 jump kinetics for each maturity group. Normality of data were assessed using the Shapiro-Wilk  
218 test. Reliability was assessed using a one-way analysis of variance (ANOVA) to test for any  
219 systematic bias, intraclass correlation coefficients (ICC) was used for relative reliability, and  
220 mean coefficients of variation (CV) used for random error. An ICC greater than 0.75 was used  
221 to identify good or excellent reliability (15), with a CV  $<$  10% deemed as acceptable (8).

222

223 Between-maturity group differences in force-time variables were assessed using a one-way  
224 ANOVA, and post-hoc analysis was used to identify any significantly between-maturity group  
225 differences using either Bonferroni or Games-Howell tests, where equal variances were or were  
226 not assumed, respectively. Cohen's *d* effect sizes were calculated using pooled standard  
227 deviations to establish the magnitude of any between-maturity group differences using the  
228 following classifications: trivial  $<$  0.19; small 0.20 – 0.59; 0.60 – 1.19 moderate; 1.20 – 1.99  
229 large; 2.0 – 3.99 very large;  $>$  4.0 extremely large (13). For variables that were not normally  
230 distributed, a Mann-Whitney effect size (*r*) was used to assess the magnitude of difference  
231 across each variable between maturity groups using the following thresholds:  $<$  0.10 (trivial),  
232 0.10 - 0.29 (small), 0.30 - 0.49 (moderate) and  $>$  0.50 (large).

233

234 Relationships between muscle architecture characteristics and maximal rebound jump kinetics  
235 for the whole sample were assessed via Pearson's correlation coefficients ( $r$ ) and interpreted  
236 using the following classifications:  $< 0.20$  no relationship;  $0.20 - 0.44$  weak;  $0.45 - 0.69$   
237 moderate;  $> 0.70$  (30). Stepwise multiple regression analyses were employed to establish the  
238 influence of muscle architecture on maximal rebound jump kinetics. All significance values  
239 were accepted at  $p < 0.05$  and all statistical procedures were conducted using SPSS v.26 for  
240 Macintosh.

241

## 242 RESULTS

### 243 **Within-session reliability**

244 Data for maximal rebound jump kinetics showed moderate to excellent relative reliability (ICC  
245 =  $0.59 - 0.98$ ) for all maturity groups and acceptable absolute reliability (CV  $< 10\%$ ) for contact  
246 time, jump height, spring like behaviour, impulse measures, and velocities within the pre-,  
247 circa-, and post-PHV cohorts. However, a number of variables across all maturity groups  
248 exceeded the acceptance threshold (CV  $> 10\%$ ), including RSI, peak GRF, RFD, peak centre  
249 of mass (COM) displacement and vertical stiffness (see supplementary *tables 1-3*).

250

### 251 **Between-maturity group differences**

252 Between-maturity group differences for maximal rebound jump kinetics are displayed in *table*  
253 *3*. There were moderate to large, significant differences between all maturity groups for peak  
254 GRF, net impulse, braking and propulsive impulse, and eccentric and concentric average power  
255 ( $d = 0.73 - 2.67$ ;  $p < 0.05$ ). There were also moderate, significant differences between pre- and  
256 circa-, and pre- and post-PHV groups for jump height and RFD ( $d = 0.64 - 1.10$ ;  $p < 0.05$ ),  
257 while eccentric velocity had small to moderate significant differences between circa- to post-,  
258 and pre- to post-PHV ( $d = 0.51$  and  $0.83$ , respectively;  $p < 0.05$ ). RSI, concentric velocity, and

259 peak COM displacement ( $d = 0.55 - 0.67$ ;  $p < 0.05$ ). were significantly different only between  
260 pre- to post-PHV groups. No significant between-maturity group differences were evidenced  
261 for contact time, eccentric time, concentric time, vertical stiffness, and spring like behaviour.

262

263 Linear regression of log transformed peak force and bodyweight data computed an allometric  
264 scaling component of 0.93 to control for the relationship between body size and relative force  
265 ( $r = -0.001$ ;  $p > 0.05$ ). Using the allometrically scaled data, there were no significant  
266 differences between maturity groups for relative peak force or relative propulsive impulse.  
267 However, relative eccentric and concentric average power, and relative braking impulse were  
268 significantly greater in the post-PHV group compared to pre-PHV group ( $d = 0.64 - 0.93$ ;  $p <$   
269  $0.05$ ).

270

271 **\*\*\* Table 3 inserted near here \*\*\***

272

### 273 **Relationships between muscle architecture and maximal rebound jump kinetics**

#### 274 *Muscle Thickness*

275 Both resting GM and VL muscle thickness demonstrated a weak to moderate association with  
276 jump height, peak GRF, total impulse, net impulse, braking impulse, propulsive impulse,  
277 eccentric and concentric average power, and eccentric velocity ( $r = 0.237 - 0.690$ ;  $p < 0.05$ ).

278 Additionally, there were moderate, negative relationships between both GM and VL muscle  
279 thickness and relative eccentric and concentric velocity ( $r = -0.471 - -0.585$ ;  $p < 0.05$ ).

280

#### 281 *Pennation Angle*

282 Resting GM pennation angle had weak associations with contact time, jump height, peak GRF,  
283 RFD, all absolute impulse measures, eccentric and concentric average power, concentric

284 velocity, and relative braking impulse ( $r = 0.230 - 0.440$ ;  $p < 0.05$ ). Resting VL pennation  
285 angle also demonstrated weak associations with total impulse, and braking and propulsive  
286 impulse ( $r = 0.200 - 0.262$ ;  $p < 0.05$ ).

287

### 288 *Fascicle Length*

289 Resting GM fascicle length showed weak associations with peak GRF, total and net impulse,  
290 propulsive impulse, eccentric and concentric average power, and eccentric velocity ( $r = 0.200$   
291  $- 0.351$ ;  $p < 0.05$ ). Resting VL fascicle length demonstrated a weak association with RSI, peak  
292 GRF, total and net impulse, propulsive impulse, eccentric and concentric average power,  
293 eccentric velocity, and both relative concentric average power ( $r = 0.200 - 0.390$ ;  $p < 0.05$ ).

294

### 295 **Regression Analyses**

296 Muscle thickness alone explained between 38.5-55.8% in peak GRF, absolute impulse  
297 variables, and concentric and eccentric average power (see table 4). However, less variance  
298 was explained in contact time (GM pennation angle - 6.7%), jump height (VL muscle thickness  
299 - 6.1%), RSI (VL fascicle length - 4.2%), RFD (VL muscle thickness - 17.2%) eccentric  
300 velocity (VL muscle thickness - 7.3%), concentric velocity (GM pennation angle - 8.5%) and  
301 relative measures (3.3-11.2%) (see table 4).

302

303 **\*\*\* Table 4 inserted near here\*\*\***

304

### 305 DISCUSSION

306 The aims of the current study were to investigate maturation effects on maximal rebound jump  
307 kinetics and determine the strength of relationships between muscle architecture characteristics  
308 and maximal rebound jump kinetics in young boys. Maximal rebound jump kinetics were

309 reduced in the pre-PHV cohort compared with the post-PHV group. Furthermore, the current  
310 study found that muscle thickness of the GM or VL predicted the variance (3.3% - 55.8%) of  
311 a number of kinetic variables during maximal rebounding in young boys. The current study  
312 results indicate that the naturally occurring changes in musculature architecture during  
313 maturation are the key determinant to maximal rebounding kinetic performance. Specifically,  
314 the majority of kinetic variables were greater in the more mature group compared to the less  
315 mature groups, and muscle thickness was the best predictor of a number of these kinetic  
316 variables.

317

318 Jump height during maximal rebound jumping was reduced in the pre-PHV group compared  
319 to the more mature cohorts. Similarly, post-PHV athletes had a greater RSI than the pre-PHV  
320 group. However, there were no differences in contact times between the groups, indicating that  
321 the increases in RSI were likely due to increased jump heights. While the reliability data from  
322 the current study states the CV values for RSI were above the 10% threshold, the differences  
323 between the pre- and circa- and pre- and post-PHV groups were larger than the typical error in  
324 the quantification of these outcomes, therefore the between-maturity group differences can be  
325 interpreted with greater confidence. However, caution should be applied when interpreting  
326 rebound jump performance difference in RSI between the circa- and post-PHV groups, as the  
327 difference was less than the typical error reported.

328

329 While VL muscle thickness explained the greatest amount of variance in jump height, and VL  
330 fascicle length was the best predictor of RSI, the explained variance of these were very low  
331 (6.7% and 4.2% respectively). These results corroborate prior literature, where VL muscle  
332 thickness and fascicle length were significantly correlated with CMJ jump height in post-PHV  
333 boys (33). Additionally, VL fascicle length correlates with maximal sprint speed in pre- and

334 post-PHV boys (33). Therefore, these findings may support the notion that VL fascicle length  
335 may have limited influence on rapid force production, or force production at high speeds.  
336  
337 Peak GRF, impulse measures, and both eccentric and concentric average power during  
338 maximal rebounding were increased across each successive maturity group. The large between  
339 group effect relative to typical error in measurement increased confidence with these between-  
340 maturity group differences. The differences in rebound performance variables between  
341 maturity groups may in part be due to the morphological and neural adaptations that manifest  
342 during growth and maturation (9, 32). Force production is generally directly proportional to  
343 muscle size (38), which increases as a result of growth and development (16, 32). The  
344 assumptions of increased force production due to increased muscle size are supported by the  
345 regression analyses from the current study, highlighting the importance of muscle thickness for  
346 explaining variance in maximal rebounding kinetics. Specifically, GM muscle thickness  
347 explained 36.9% of peak GRF, between 40.2–47.2% of variance in net, braking and propulsive  
348 impulse, and 36.0% and 32.0% eccentric and concentric average power, respectively.  
349 Furthermore, when VL muscle thickness was added to the regression model, the explained  
350 variance increased to 44.4% for peak GRF, between 44.6–55.8% for impulse variables, 43.3%  
351 of eccentric average power and 38.5% of concentric average power. The association between  
352 peak force during jumping and muscle thickness of the knee and ankle extensors reported in  
353 adolescent surfers (36), showed that lateral gastrocnemius and vastus lateralis thickness  
354 predicted 44% and 45% of peak force in a CMJ. Additionally, the relationship between muscle  
355 thickness and power output during jumping is similar to previous findings, albeit in adults,  
356 where muscle thickness of the gastrocnemius explained 20% of the variance in peak power of  
357 a CMJ (11). Cumulatively, the current findings indicate that muscle thickness of the ankle and

358 knee extensors are important determinants for force and power production during jumping  
359 tasks in young boys.

360

361 RFD was greater in both post- and circa-PHV compared with the pre-PHV group, and these  
362 the effect sizes exceeded the typical error reported from the reliability data. Furthermore, VL  
363 muscle thickness predicted 17.4% of the variance in RFD. Considering that maximal strength  
364 is correlated with RFD (25) and that muscle size influences maximal strength (14, 38), this  
365 reported effect is not unexpected. Gastrocnemius thickness is similarly associated with later  
366 RFD (30-50 ms) during a drop jump in adults (10). However, it should be noted that in the  
367 current study, the explained variance of RFD was relatively low ( $R^2 = 17.4\%$ ) and adding GM  
368 muscle thickness to the model only increased the explained variance to ~20%, indicating that  
369 there are a number of additional factors that underlie RFD in children, such as tendon stiffness  
370 and muscle activation rate (40). Considering that muscles containing longer fascicles may have  
371 the capability to produce force at higher shortening velocities due to a greater number of  
372 sarcomeres in series (2, 19), the lack of association between fascicle length and RFD is  
373 somewhat surprising. The lower association between muscle architecture and RFD may also  
374 be due to the greater typical errors associated with RFD which in the current study ranged  
375 between 20.4% - 25%. These coefficients of variation are consistent with previous research in  
376 young athletes (27). However, in adults, research has highlighted that gastrocnemius fascicle  
377 length has an inverse relationship with early RFD (0-10ms) during drop jumps (10). This may  
378 be due to series elastic compliance residing largely in the cross-bridges and myofilaments (4),  
379 and therefore an increased fascicle length with more cross-bridges may result in greater  
380 compliance, which may actually reduce RFD (4).

381

382 GM pennation angle explained a small amount of variance in both concentric velocity (8.5%)  
383 and contact time (7.2%). Contact time is a surrogate for contraction rate, and the distance  
384 moved during that time will determine the velocity. Interestingly, VL muscle thickness  
385 explained a small amount of variance in eccentric velocity (7.3%). A faster eccentric velocity  
386 increases neuromuscular activation during a SSC due to an increased stretch reflex and  
387 musculo-tendon stiffness (10). Therefore, it may be of interest in future studies to identify the  
388 relationship between muscle architecture variables and muscle activation properties during  
389 maximal rebounding. Ultimately, there was a large amount of unexplained variance in  
390 movement velocity. This may be due to a number of factors, including changes in  
391 biomechanical strategies. When compared to pre-PHV boys, post-PHV boys increased their  
392 ground contact time by ~9%, but COM displacement increased by nearly 30% during this  
393 ground contact period, resulting in increased movement velocity. This may reflect changing  
394 neuromuscular control strategies with advancing maturation, with more mature subjects  
395 favouring longer contact durations to develop an increased net impulse, and greater COM  
396 displacement during ground contact to favour increased velocity.

397

398 While the majority of absolute measures showed moderate to large differences across maturity  
399 in the current cohort of young boys, when these measures were normalized relative to body  
400 mass, the differences were reduced. Relative braking impulse, and relative eccentric and  
401 concentric average power were all greater in the post-PHV group compared with the pre-PHV  
402 group, but there were no differences between maturity groups for relative peak force or relative  
403 propulsive impulse. Furthermore, there was limited explained variance in any relative measure  
404 (< 11.2%) highlighting that muscle architecture has a fixed influence on relative measure  
405 during maximal rebound jumping. Therefore, increases in absolute force, impulse, and power



406 are likely to be most influenced by an increased body mass during maturation in developing  
407 young boys.

408

409 The findings from the current study demonstrate the importance of the GM during maximal  
410 rebounding, as GM muscle architecture was the best predictor of 11 maximal rebounding  
411 kinetic variables (6.7% - 47.2%). This is in contrast to the VL, which explained the most  
412 variance in six variables, all with a small amount of explained variance (3.3% - 7.8%). The  
413 current study results conflicts with previous findings for CMJ performance in young boys,  
414 where there was a greater emphasis from musculature around the knee joint (33). Considering  
415 that vertical rebounding relies heavily on the *triceps surae* musculature (18), it can be  
416 postulated that as athletes mature and develop appropriate musculature at the ankle joint (16,  
417 32), they can begin to utilise distal joint kinetics to a greater effect during maximal rebounding.

418

419 The results of this study are one of the first to report differences in maximal rebounding kinetics  
420 across various different maturity groups and identified their relationships with muscle  
421 architecture variables, however results should be interpreted in light of certain limitations.  
422 Considering that muscle geometry is not fixed for a given muscle and dynamic changes occur  
423 during a contraction, the visualization of architecture in non-contracted, static muscle may not  
424 allow inference of complete muscle function during dynamic, active movements. Therefore,  
425 future research may need to study the role of muscle in a more dynamic nature, and the role  
426 that this has on SSC performance. Additionally, while the current study provides insight into  
427 the relationships between muscle architecture and SSC performance, the effects of training on  
428 muscle architecture measures are still unknown and provide a unique opportunity for further  
429 research in light of the current study results. highlighting the role that muscle architecture of  
430 the GM and VL muscles have on maximal rebounding kinetics in youth.

431

## 432 PRACTICAL APPLICATIONS

433 The current data indicate that muscle thickness of the GM influences maximal rebounding  
434 ability in young boys. Therefore, increasing lower limb muscle mass is an important  
435 determinant to positively influence maximal rebounding kinetics in young males. Additionally,  
436 the findings suggest that maximal rebounding performance is dictated to a larger extent by the  
437 musculature around the ankle joint. From a training perspective, if the goal of training is to  
438 increase maximal rebounding performance, it may be prudent for practitioners to include  
439 exercises that target the hypertrophy of the gastrocnemius muscle within the training  
440 programmes of male youth. While the influence of specific training methods on the  
441 development of unique muscle architecture changes is still unknown in paediatric populations,  
442 previous studies in adults highlight that heavy resistance training may enhance muscle  
443 thickness (3) and hypertrophy in young males.

444

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559

**Table 1.** Descriptive statistics for all anthropometric variables for the pre-PHV, circa-PHV and post-PHV groups (mean  $\pm$  SD)

	Pre-PHV (n = 45)	Circa-PHV (n = 25)	Post-PHV (n = 29)
Age (years)	12.47 $\pm$ 0.54	13.85 $\pm$ 0.75	15.76 $\pm$ 0.82
Standing Height (cm)	153.16 $\pm$ 6.53	167.14 $\pm$ 5.12	177.57 $\pm$ 6.08
Leg Length (cm)	75.92 $\pm$ 5.00	82.09 $\pm$ 4.38	83.89 $\pm$ 4.17
Body Mass (kg)	42.59 $\pm$ 6.40	56.88 $\pm$ 9.13	72.83 $\pm$ 12.89
Maturity Offset (years)	-1.67 $\pm$ 0.44	-0.01 $\pm$ 0.28	2.07 $\pm$ 0.61

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561

**Table 2.** Method of calculation for all maximal rebound jumping kinetics

<b>VARIABLE</b>	<b>METHOD OF CALCULATION</b>
<b>Ground Contact Time (s)</b>	Take-off and landing points were identified as the first data point recorded greater than 15 N (initial ground contact) and the final data point above 15 N (take-off). Using these time points, the “noise” of the flight time force was calculated. A threshold of 5*SD was calculated and this was used as the threshold for determining actual take-off and landing. The duration of time between landing and take-off was defined as ‘ground contact time’
<b>Jump Height (m)</b>	Defined as the largest vertical displacement of the body’s centre of mass during the flight time between the first and second ground contact  $= TOV^2/2g$  (TOV = take off velocity; g = acceleration due to gravity)
<b>Reactive Strength Index</b>	Calculated as the ratio of jump height (mm) and ground contact time (ms)
<b>Peak Ground Reaction Force (N)</b>	Calculated as the highest force peak during each maximal hop
<b>Peak Instantaneous Rate of Force Development (N/s)</b>	Defined as the 0.001 s interval that had the greatest change in force between initial ground contact and the occurrence of the first peak.
<b>Total Impulse (N.s)</b>	Total vertical impulse applied to the ground during ground contact is calculated by summing the instantaneous impulse values (force x time) for the duration of the ground contact during each hop.
<b>Net Impulse (N.s)</b>	Net vertical impulse is the difference produced by subtracting body weight impulse from the total vertical impulse.
<b>Braking Impulse (Ns)</b>	Braking impulse (is the total vertical impulse applied to the ground during the landing phase of ground contact and is calculated by summing the instantaneous impulse values between initial ground contact and peak centre of mass displacement.
<b>Propulsive Impulse (Ns)</b>	Concentric impulse is the total vertical impulse applied to the ground during the take-off phase of ground contact and is calculated by summing the instantaneous impulse values between peak centre of mass displacement and take-off.

<b>Eccentric Average Power (W)</b>	Velocity of the centre of mass was multiplied by the ground reaction force at each timing sample to derive power. Mean eccentric power was calculated as the average power between initial ground contact and the timing of the maximal displacement of centre of mass.
<b>Concentric Average Power (W)</b>	Velocity of the centre of mass was multiplied by the ground reaction force at each timing sample to derive power. Mean concentric power was calculated as the average power from the timing of lowest point of the centre of mass and the point of take-off.
<b>Spring like Correlation (r)</b>	Determined by calculating a Pearson's correlation of coefficient using centre of mass displacement and absolute vertical force throughout the initial ground contact.
<b>Vertical Stiffness (KN/m)</b>	Vertical stiffness is calculated as the ratio of peak vertical ground reaction force during the first landing to maximal vertical displacement of the centre of mass. Since the calculation of stiffness relies on the assumption that an individual is displaying spring-like characteristics and that peak force and peak displacement occur at the same time, previous literature has utilised a threshold of -0.8 for the Pearson correlation between vertical force and vertical displacement to indicate spring-like behaviour. If the Pearson correlation is greater than -0.8 then stiffness is not calculated.
<b>Peak Centre of Mass Displacement (m)</b>	Determined by dividing the vertical component of the ground reaction force by the participant's body mass to determine acceleration. Double integration of acceleration was then performed to calculate displacement of centre of mass.
<b>Relative peak Ground Reaction Force (N/kg)</b>	Peak ground reaction force divided by allometrically scaled body mass
<b>Relative Braking Impulse (N.s/kg)</b>	Braking impulse divided by allometrically scaled body mass
<b>Relative Propulsive Impulse (N.s/kg)</b>	Propulsive impulse divided by allometrically scaled body mass
<b>Relative Eccentric Average Power (W/kg)</b>	Eccentric average power divided by allometrically scaled body mass
<b>Relative Concentric Average Power (W/kg)</b>	Concentric average power divided by allometrically scaled body mass

**Table 3.** Differences in maximal rebounding kinetics across maturity groups

	<b>PRE</b>	<b>CIRCA</b>	<b>POST</b>	<b>EFFECT SIZE (<i>d</i>)</b>		
	Mean $\pm$ SD	Mean $\pm$ SD	Mean $\pm$ SD	PRE - CIRCA	CIRCA - POST	PRE - POST
<b>Contact time (s)</b>	0.23 $\pm$ 0.07	0.24 $\pm$ 0.07	0.25 $\pm$ 0.09	0.11	0.13	0.23
<b>Jump height (m)</b>	0.21 $\pm$ 0.05	0.25 $\pm$ 0.05*	0.28 $\pm$ 0.08*	0.74	0.44	0.99
<b>RSI</b>	1.00 $\pm$ 0.28	1.14 $\pm$ 0.37	1.25 $\pm$ 0.49*	0.45	0.24	0.63
<b>Peak GRF (N)</b>	2162 $\pm$ 481	2964 $\pm$ 772*	3666 $\pm$ 821*#	1.10	0.73	1.99
<b>Peak Instantaneous RFD (N/s)</b>	56939 $\pm$ 22488	77021 $\pm$ 23535*	90327 $\pm$ 28660*	0.81	0.49	1.12
<b>Total Impulse (N.s)</b>	266.8 $\pm$ 51.3	379.6 $\pm$ 69.6*	516.8 $\pm$ 134.0*#	1.42	1.07	1.63
<b>Net Impulse (N.s)</b>	171.6 $\pm$ 25.4	249.4 $\pm$ 45.7*	338.5 $\pm$ 80.8*#	1.54	1.11	1.70
<b>Braking Impulse (N.s)</b>	122.9 $\pm$ 27.8	179.1 $\pm$ 31.2*	249.0 $\pm$ 69.8*#	1.42	1.08	1.61
<b>Propulsive Impulse (N.s)</b>	145.0 $\pm$ 29.7	205.7 $\pm$ 48.3*	272.6 $\pm$ 69.0*#	1.22	0.98	1.58
<b>Peak CoM displacement (m)</b>	0.14 $\pm$ 0.05	0.17 $\pm$ 0.05	0.18 $\pm$ 0.06*	0.50	0.32	0.76
<b>Spring like behaviour</b>	0.92 $\pm$ 0.07	0.91 $\pm$ 0.10	0.93 $\pm$ 0.06	-0.18	0.27	0.13
<b>Vertical Stiffness (kN/m)</b>	19.38 $\pm$ 10.84	23.35 $\pm$ 10.28	24.25 $\pm$ 12.09	0.37	0.08	0.42
<b>Eccentric Average Power (W)</b>	1417 $\pm$ 292	2102 $\pm$ 600*	2895 $\pm$ 881*#	1.33	0.92	2.15
<b>Concentric Average Power (W)</b>	1399 $\pm$ 324	2102 $\pm$ 662*	2897 $\pm$ 703*#	1.23	0.79	1.83
<b>Eccentric Velocity (m/s)</b>	1.06 $\pm$ 0.14	1.11 $\pm$ 0.17*	1.22 $\pm$ 0.19*	0.27	0.51	0.83
<b>Concentric Velocity (m/s)</b>	1.19 $\pm$ 0.21	1.32 $\pm$ 0.26	1.36 $\pm$ 0.26*	0.49	0.13	0.64
<b>Relative peak GRF (N/kg<sup>0.93</sup>)</b>	66.10 $\pm$ 11.59	69.00 $\pm$ 13.64	68.86 $\pm$ 15.44	0.19	-0.01	0.17



<b>Relative braking impulse (N.s/ kg<sup>0.93</sup>)</b>	3.76 ± 0.65	4.21 ± 0.65	4.57 ± 0.81*	0.57	0.42	0.93
<b>Relative propulsive impulse (N.s/ kg<sup>0.93</sup>)</b>	4.61 ± 0.79	4.82 ± 0.96	5.05 ± 0.95	0.20	0.20	0.42
<b>Relative eccentric average power (W/ kg<sup>0.93</sup>)</b>	43.55 ± 8.11	49.05 ± 11.78	53.95 ± 14.56*	0.47	0.31	0.79
<b>Relative concentric average power (W/ kg<sup>0.93</sup>)</b>	43.23 ± 9.79	49.23 ± 13.93	54.40 ± 20.44*	0.43	0.26	0.64

RSI: Reactive strength index; GRF: ground reaction force; RFD: Rate of force development; CoM: centre of mass

\*significantly greater than pre-PHV

# significantly greater than circa-PHV

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**Table 4.** Explained variance of maximal hopping kinetics from muscle architecture variables

<b>Dependent Variable</b>	<b>Model Number</b>	<b>Independent Variable</b>	<b>Adjusted R<sup>2</sup> (%)</b>	<b>Model p value</b>
Peak GRF (N)	1	GMMT	36.9	< 0.001
	2	GMMT + VLMT	44.4	< 0.001
Peak Instantaneous RFD (N.s <sup>-1</sup> )	1	VLMT	17.4	< 0.001
	2	VLMT + GMMT	19.8	0.032
Net Impulse (N.s)	1	GMMT	47.2	< 0.001
	2	GMMT + VLMT	55.8	< 0.001
Braking Impulse (N.s)	1	GMMT	40.2	< 0.001
	2	GMMT + VLMT	44.6	0.001
	3	GMMT + VLMT + GMFL	47.4	0.007
	4	GMMT + VLMT + GMFL + VLFL	48.9	0.032
Propulsive Impulse (N.s)	1	GMMT	42.1	< 0.001
	2	GMMT + VLMT	48.7	0.001
Eccentric Average Power (W)	1	GMMT	36.0	< 0.001
	2	GMMT + VLMT	43.3	< 0.001
Concentric Average Power (W)	1	GMMT	32.0	< 0.001
	2	GMMT + VLMT	38.5	0.001
Eccentric Velocity (m/s)	1	VLMT	7.3	0.001
Concentric Velocity (m/s)	1	GMPA	8.5	0.001
Relative Braking Impulse (N.s/kg)	1	GMPA	11.2	< 0.001
Relative Eccentric Average Power (W/kg)	1	VLMT	3.3	0.022
Relative Concentric Average Power (W/kg)	1	VLFL	7.8	0.001

GM: Gastrocnemius Medialis; VL: Vastus Lateralis; MT: Muscle Thickness; PA: Pennation Angle; FL: Fascicle Length